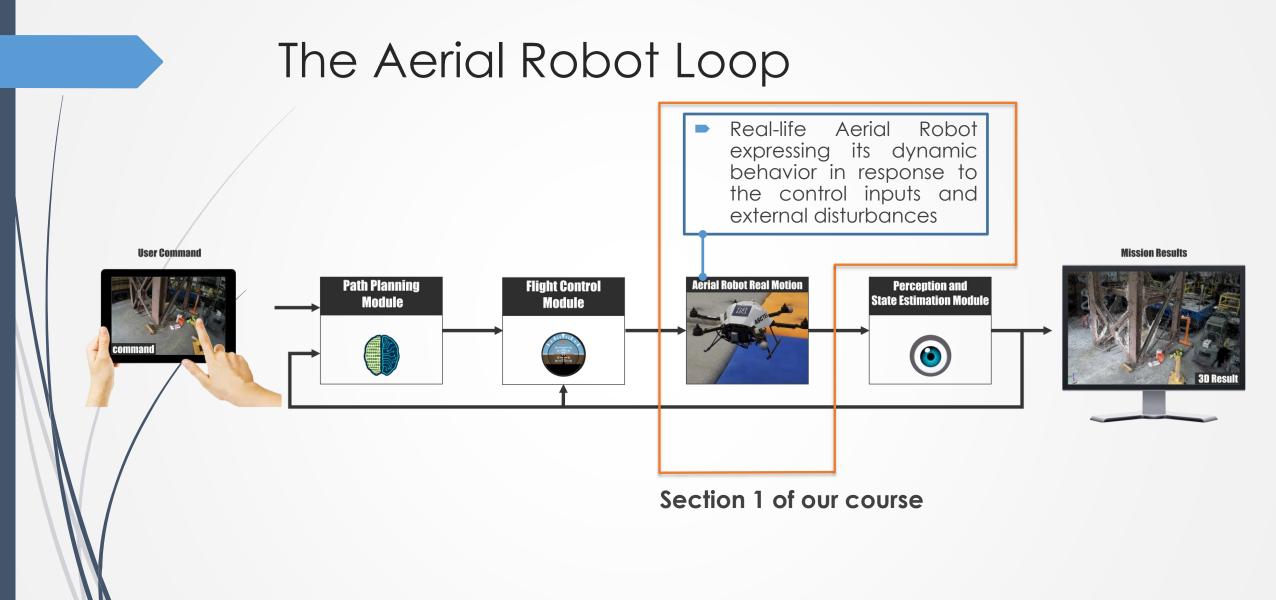


CS491/691: Introduction to Aerial Robotics Topic: Micro Aerial Vehicle Dynamics

Dr. Kostas Alexis (CSE)



Goal of this lecture

- The goal of this lecture is to derive the equations of motion that describe the motion of a multirotor Micro Aerial Vehicle.
- The MAV has 6 Degrees of Freedom but only 4 distinct inputs.
 - It is an underactuated system.
 - To achieve this goal, we rely on:
 - A model of the Aerodynamic Forces & Moments
 - A model of the motion of the vehicle body as actuated by the forces and moments acting on it.



- The goal of this lecture is to derive the equations of motion that describe the motion of a multirotor Micro Aerial Vehicle.
- To achieve this goal, we rely on:
 - A model of the Aerodynamic Forces & Moments
 - A model of the motion of the vehicle body as actuated by the forces and moments acting on it.







Is something much simpler than a helicopter rotor





Video of airflow and vortex patterns with propellers. These tests were conducted at NACA, now NASA Langley Research Center. The interior tests were probably at the Propeller Research Tunnel. The exterior tests at the end of the film were at the Helicopter Test Tower. Langley Film #L-118

- Rotor modeling is a very complicated process.
- A Rotor is different than a propeller. It is not-rigid and contains degrees of freedom. Among them blade flapping allows the control of the rotor tip path plane and therefore control the helicopter.



- Used to produce thrust.
- Propeller plane perpendicular to shaft.
- Rigid blade. No flapping.
- Fixed blade pitch angle or collective changes only.



- Used to produce lift and directional control.
- Elastic element between blade and shaft.
- Blade flapping used to change tip path plane.
- Blade pitch angle controlled by swashplate.





- In a simplified assumption, a propeller is considered to present no blade flapping.
- It is approximated as a rotor disc producing thrust and drag forces.
- Thrust & Power Equations

$$F_{Thrust} = \frac{1}{2}\rho A v^2$$
$$P = \frac{1}{2}Av^2$$

Hover case (ideal power):

$$P = \frac{F_{Thrust}^{3/2}}{\sqrt{2\rho A_R}} = \frac{(mg)^{3/2}}{\sqrt{2\rho A_R}}$$

V, A_o, p	\mathcal{P}_0
	0
	T / /
$V+u_1, A_R, p_1$	1
$V + u_{21} A_{R}, p_{2}$	2
$V+u_3$, A_R , p_3	3

Thrust & Power Equations

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• Figure of Merit:

$$FM = \frac{Ideal \ Power \ to \ Hover}{Real \ Power \ to \ Hover}$$

RI

 V, A_o, p_o

 $V+u_{I}, A_{R}, p_{I}$

 $V + u_{2} A_{R}, p_{2}$

 $V + u_{3}, A_{R}, p_{3} = 3$

2

Lift & Drag at Blade Element:

$$dL = \frac{\rho}{2} C_L cdr V^2 \qquad dD = \frac{\rho}{2} C_L cdr V^2$$

$$dT = N_b (dL \cos \phi - dD \sin \phi)$$

$$dQ = N_b (dL \sin \phi - dD \cos \phi)r$$

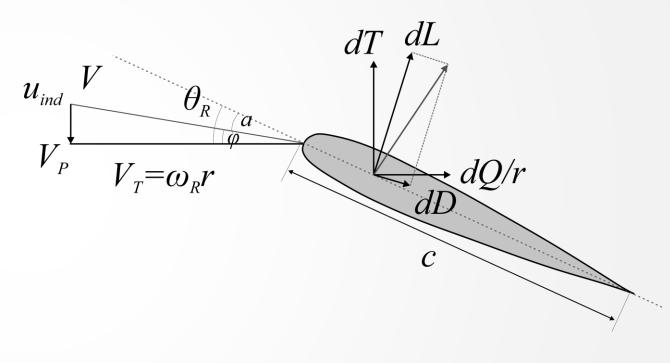
$$V \approx V_T \qquad \phi \approx \frac{V'_P}{V_T}$$

$$dT \approx N_b dL$$

$$C_L = C_{L\alpha} (\alpha - \alpha_0)$$

$$C_{L\alpha} = 2\pi$$

- $C_{L\alpha} = 5.7$
- A0: zero lift angle of attack.
- Linearize polar for Reynolds number at 2/3 R $dT_{be} = N_b \frac{\rho}{2} C_{L\alpha} (\theta_R - \frac{V_P}{V_T} - \alpha_0) cdr V_T^2$



- Simplified model forces and moments:
 - Thrust Force: the resultant of the vertical forces acting on all the blade elements.

 $F_T = T = C_T \rho A (\Omega R)^2$

Hub Force: the resultant of all the horizontal forces acting on all the blade elements.

 $F_H = H = C_H \rho A (\Omega R)^2$

Drag Moment: This moment about the rotor shaft is caused by the aerodynamic forces acting on the blade elements. The horizontal forces acting on the rotor are multiplied by the moment arm and integrated over the rotor. Drag moment determines the power required to spin the rotor.

 $M_Q = Q = C_Q \rho A (\Omega R)^2 R$

What is the relation between the propeller aerodynamic forces and moments, the gravity force and the motion of the aerial robot?

MAV Dynamics

 T_6

 \mathcal{Q}_{3}

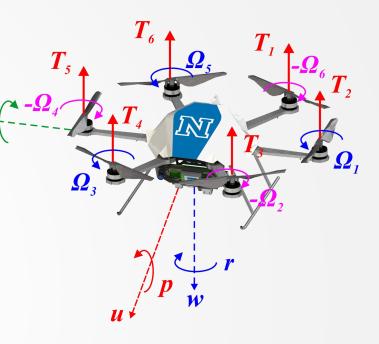
- Assumption 1: the Micro Aerial Vehicle is flying as a rigid body with negligible aerodynamic effects on it – for the employed airspeeds.
 - The propeller is considered as a simple propeller disc that generates thrust and a moment around its shaft.

Recall:

$$F_T = T = C_T \rho A (\Omega R)^2$$
$$M_Q = Q = C_Q \rho A (\Omega R)^2 R$$

And let us write:

$$T_i = k_n \Omega_i^2$$
$$M_i = (-1)^{i-1} k_m T_i$$



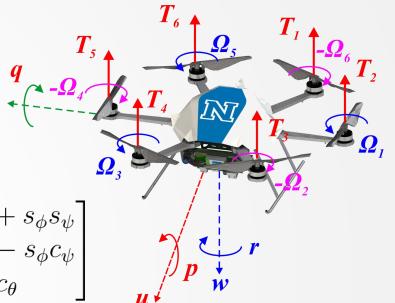
Recall the kinematic equations:

Translational Kinematic Expression:

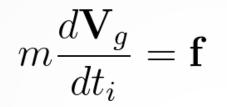
$$\begin{bmatrix} \dot{p}_n \\ \dot{p}_e \\ \dot{p}_d \end{bmatrix} = \mathcal{R}_b^v \begin{bmatrix} u \\ v \\ w \end{bmatrix}, \ \mathcal{R}_b^v = \begin{bmatrix} c_\theta c_\psi & s_\phi s_\theta c_\psi - c_\phi s_\psi & c_\phi s_\theta c_\psi + s_\phi s_\psi \\ c_\theta s_\psi & s_\phi s_\theta s_\psi + c_\phi c_\psi & c_\phi s_\theta s_\psi - s_\phi c_\psi \\ -s_\theta & s_\phi c_\theta & c_\phi c_\theta \end{bmatrix}$$

Rotational Kinematic Expression

$\left[\dot{\phi}\right]$		[1	$\sin\phi\tan\theta$	$\cos\phi\tan\theta$	$\lceil p \rceil$
$\dot{ heta}$	=	0	$\cos\phi$	$-\sin\phi$	q
$\dot{\psi}$		0	$\sin\phi\sec\theta$	$\cos\phi\sec\theta$	$\lfloor r \rfloor$



• Recall Newton's 2nd Law:



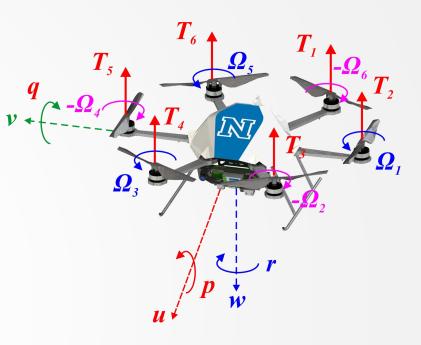
f is the summary of all external forces

- m is the mass of the robot
- Time derivative is taken wrt the interial frame
- Using the expression:

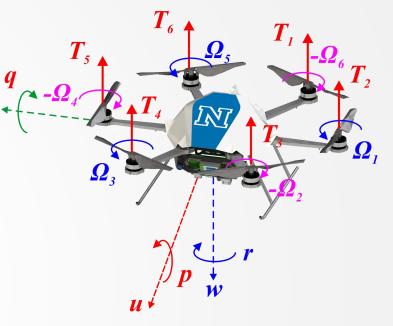
$$\frac{d\mathbf{V}_g}{dti} = \frac{d\mathbf{V}_g}{dt_b} + \omega_{b/i} \times \mathbf{V}_g \quad \Longrightarrow \quad m(\frac{d\mathbf{V}_g}{dt_b} + \omega_{b/i} \times \mathbf{V}_g) = \mathbf{f}$$

Which expressed in the body frame:

$$m(\frac{d\mathbf{V}_g^b}{dt_b} + \omega_{b/i}^b \times \mathbf{V}_g^b) = \mathbf{f}^b$$



$$\begin{split} & \mathsf{MAV Dynamics} \\ & m(\frac{d\mathbf{V}_g^b}{dt_b} + \omega_{b/i}^b \times \mathbf{V}_g^b) = \mathbf{f}^b \\ & \mathsf{W} \mathsf{here} \\ & \mathbf{V}_g^b = \begin{bmatrix} u \\ v \\ w \end{bmatrix}, \ \omega_{b/i}^b = \begin{bmatrix} p \\ q \\ r \end{bmatrix}, \mathbf{f}^b = \begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix} \\ & \mathsf{Therefore:} \\ & \begin{bmatrix} \dot{u} \\ \dot{v} \\ \dot{w} \end{bmatrix} = \begin{bmatrix} rv - qw \\ pw - ru \\ qu - pv \end{bmatrix} + \frac{1}{m} \begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix} \end{split}$$



• Recall Newton's 2nd Law:

 \rightarrow *h* is the angular momentum vector

 $d\mathbf{h}$

 $\overline{dt_i}$

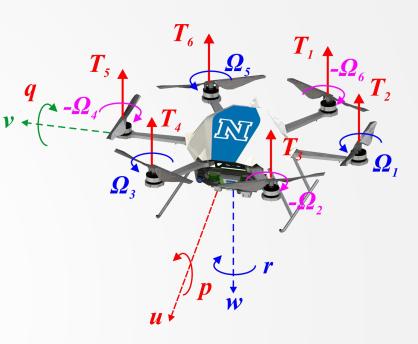
- **m** is the summary of all external moments
- Time derivative is taken wrt the interial frame
- Therefore:

$$\frac{d\mathbf{h}}{dt_i} = \frac{d\mathbf{h}}{dt_b} + \omega_{b/i} \times \mathbf{h} = \mathbf{m}$$

= m

Which expressed in the body frame:

$$\frac{d\mathbf{h}^b}{dt_b} + \omega^b_{b/i} \times \mathbf{h}^b = \mathbf{m}^b$$



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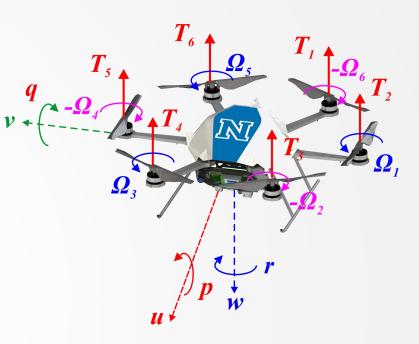
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Which expressed in the body frame:

$$\frac{d\mathbf{h}^b}{dt_b} + \omega^b_{b/i} \times \mathbf{h}^b = \mathbf{m}^b$$



For a rigid body, the angular momentum is defined as the product of the inertia matrix and the angular velocity vector:

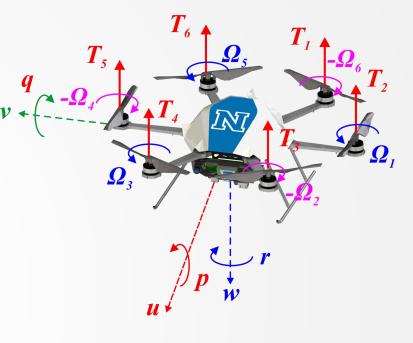
$$\mathbf{h}^b = \mathbf{J}\omega^b_{b/i}$$

where

$$\mathbf{J} = \begin{bmatrix} J_x & -J_{xy} & -J_{xz} \\ -J_{xy} & J_y & -J_{yz} \\ -J_{xz} & -J_{yz} & J_z \end{bmatrix}$$

But as the multirotor MAV is symmetric:

$$\mathbf{J} = \begin{bmatrix} J_x & 0 & 0\\ 0 & J_y & 0\\ 0 & 0 & J_z \end{bmatrix}$$



V +

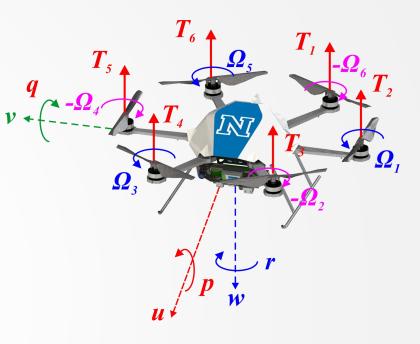
MAV Dynamics
• Replacing in:

$$\frac{d\mathbf{h}^{b}}{dt_{b}} + \omega_{b/i}^{b} \times \mathbf{h}^{b} = \mathbf{m}^{b}$$
• Gives:

$$\mathbf{J}\frac{d\omega_{b/i}^{b}}{dt_{b}} + \omega_{b/i}^{b} \times (\mathbf{J}\omega_{b/i}^{b})$$

$$\dot{\omega}_{b/i}^{b} = \mathbf{J}^{-1}[-\omega_{b/i}^{b} \times (\mathbf{J}\omega_{b/i}^{b})]$$
• where

$$\dot{\omega}_{b/i}^{b} = \mathbf{J}^{-1}[-\omega_{b/i}^{b} \times (\mathbf{J}\omega_{b/i}^{b})]$$



R

$$\mathbf{J}\frac{d\omega_{b/i}^{o}}{dt_{b}} + \omega_{b/i}^{b} \times (\mathbf{J}\omega_{b/i}^{b}) = \mathbf{m}^{b} \Rightarrow$$
$$\omega_{b/i}^{b} = \mathbf{J}^{-1}[-\omega_{b/i}^{b} \times (\mathbf{J}\omega_{b/i}^{b}) + \mathbf{m}^{b}]$$

$$\dot{\omega}_{b/i}^b = \begin{bmatrix} \dot{p} \\ \dot{q} \\ \dot{r} \end{bmatrix}$$

By setting the moments vector:

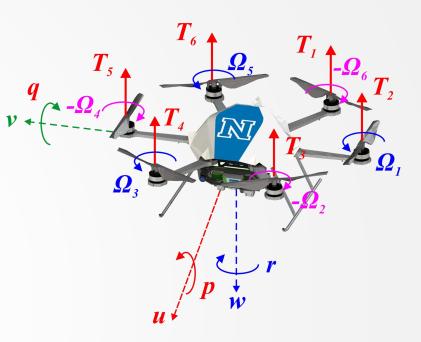
$$\mathbf{m}^b = \begin{bmatrix} M_x \\ M_y \\ M_z \end{bmatrix}$$

Then for the symmetric MAV, equation:

$$\dot{\omega}_{b/i}^b = \mathbf{J}^{-1}[-\omega_{b/i}^b \times (\mathbf{J}\omega_{b/i}^b) + \mathbf{m}^b]$$

Becomes:

$$\begin{bmatrix} \dot{p} \\ \dot{q} \\ \dot{r} \end{bmatrix} = \begin{bmatrix} \frac{J_y - J_z}{J_x} qr \\ \frac{J_z - J_x}{J_y} pr \\ \frac{J_x - J_y}{J_z} pq \end{bmatrix} + \begin{bmatrix} \frac{1}{J_x} M_x \\ \frac{1}{J_y} M_y \\ \frac{1}{J_z} M_z \end{bmatrix}$$



To append the forces and moments we need to combine their formulation with $\nu \star$

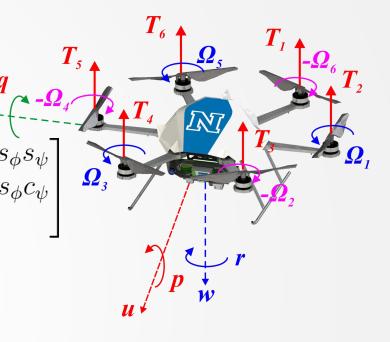
$$\begin{bmatrix} \dot{p}_n \\ \dot{p}_e \\ \dot{p}_d \end{bmatrix} = \mathcal{R}_b^v \begin{bmatrix} u \\ v \\ w \end{bmatrix}, \ \mathcal{R}_b^v = \begin{bmatrix} c_\theta c_\psi & s_\phi s_\theta c_\psi - c_\phi s_\psi & c_\phi s_\theta c_\psi + s_\theta c_\psi & s_\phi s_\theta s_\psi - s_\theta c_\psi & s_\phi s_\theta s_\psi - s_\theta c_\phi c_\psi & c_\phi s_\theta s_\psi - s_\theta c_\phi c_\theta & s_\phi c_\theta & c_\phi c_\theta \end{bmatrix}$$

$$\begin{bmatrix} \dot{u} \\ \dot{v} \\ \dot{w} \end{bmatrix} = \begin{bmatrix} rv - qw \\ pw - ru \\ qu - pv \end{bmatrix} + \frac{1}{m} \begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix}$$

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = \begin{bmatrix} 1 & \sin\phi \tan\theta & \cos\phi \tan\theta \\ 0 & \cos\phi & -\sin\phi \\ 0 & \sin\phi \sec\theta & \cos\phi \sec\theta \end{bmatrix} \begin{bmatrix} p \\ q \\ r \end{bmatrix}$$

$$Next step and momentary$$

$$\begin{bmatrix} \dot{p} \\ \dot{q} \\ \dot{r} \end{bmatrix} = \begin{bmatrix} \frac{J_y - J_z}{J_x} qr \\ \frac{J_z - J_x}{J_z} pr \\ \frac{J_x - J_y}{J_z} pq \end{bmatrix} + \begin{bmatrix} \frac{1}{J_x} M_x \\ \frac{1}{J_y} M_y \\ \frac{1}{J_z} M_z \end{bmatrix}$$



p: append the MAV forces nents

q

MAV forces in the body frame:

Jx

 f_y

 \mathbf{f}_b

Moments in the body frame:

$$\mathbf{m}_{b} = \begin{bmatrix} M_{x} \\ M_{y} \\ M_{z} \end{bmatrix} = \begin{bmatrix} lc_{60} & l & lc_{60} & -lc_{60} & -l & -lc_{60} \\ -ls_{60} & 0 & ls_{60} & ls_{60} & 0 & -ls_{60} \\ -k_{m} & k_{m} & -k_{m} & k_{m} & -k_{m} & k_{m} \end{bmatrix} \begin{bmatrix} T_{2} \\ T_{3} \\ T_{4} \\ T_{5} \end{bmatrix}$$

 $\begin{bmatrix} 0\\ \sum_{i=1}^{6} T_i \end{bmatrix}$

 T_1

 T_6

 T_6

 $\boldsymbol{\Omega}$

N

 T_{5}

 \mathcal{Q}_{3}

 $= \begin{bmatrix} 0\\ \sum_{i=1}^{6} T_i \end{bmatrix}$

MAV forces in the body frame:

 $\begin{array}{c} f_x \\ f_y \\ f_z \end{array}$

 $\mathbf{f}_b =$

Moments in the body frame:

$$\mathbf{m}_{b} = \begin{bmatrix} M_{x} \\ M_{y} \\ M_{z} \end{bmatrix} = \begin{bmatrix} lc_{60} & l & lc_{60} & -lc_{60} & -l & -lc_{60} \\ -ls_{60} & 0 & ls_{60} & ls_{60} & 0 & -ls_{60} \\ -k_{m} & k_{m} & -k_{m} & k_{m} & -k_{m} & k_{m} \end{bmatrix} \begin{bmatrix} T_{2} \\ T_{3} \\ T_{4} \\ T_{5} \end{bmatrix}$$

Bx

30°

Bz

5

 T_1

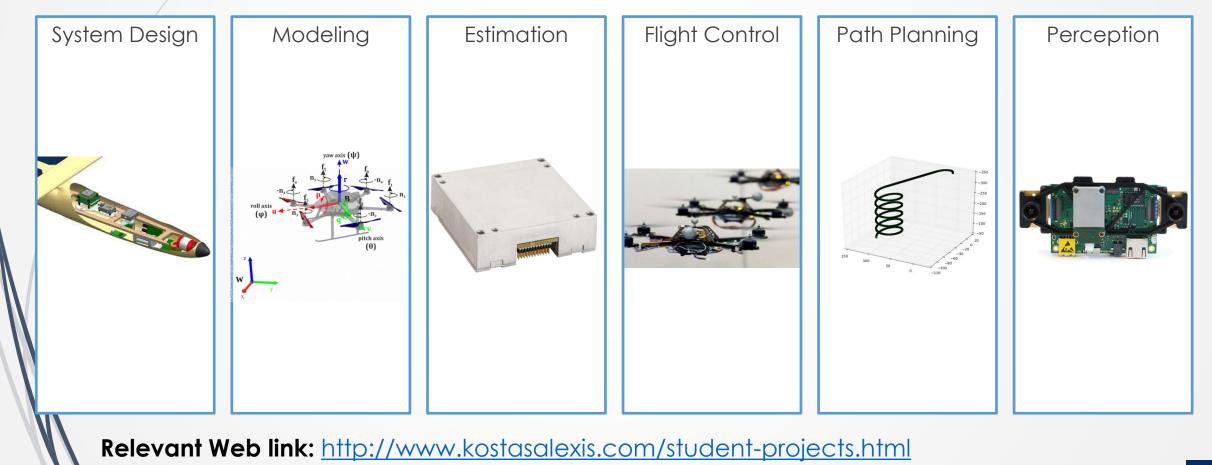
 T_6

60°

2

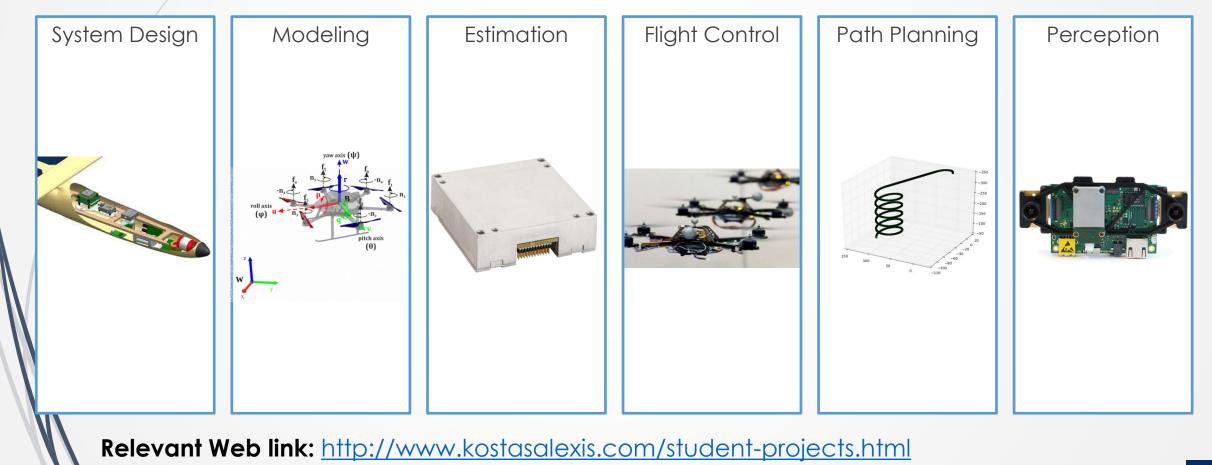
Course Projects

Assemble teams (~5 students), select or think of a Project and schedule a meeting with me



Course Projects

Assemble teams (~5 students), select or think of a Project and schedule a meeting with me



Find out more

- <u>http://www.kostasalexis.com/multirotor-dynamics.html</u>
- S. Leutenegger, C. Huerzeler, A.K. Stowers, K. Alexis, M. Achtelik, D. Lentink, P. Oh, and R. Siegwart. "Flying Robots", Handbook of Robotics (upcoming new version available upon request).
- <u>http://www.kostasalexis.com/simulations-with-simpy.html</u>

MATLAB http://www.mathworks.com/help/aeroblks/examples/quadcopterDemo:

- project.html?refresh=true
- Help with Differential Equations? <u>https://www.khanacademy.org/math/differential-equations</u>
- Always check: <u>http://www.kostasalexis.com/literature-and-links.html</u>

External Product of 2 vectors

Let:

$$\mathbf{u} = [u_1, u_2, \dots, u_m]$$

$$\mathbf{v} = [v_1, v_2, \dots, v_n]$$
Then:

$$\mathbf{u} \times \mathbf{v} = \begin{bmatrix} u_1 v_1 & u_1 v_2 & \cdots & u_1 v_n \\ u_2 v_1 & u_2 v_2 & \cdots & u_2 v_n \\ \vdots & \vdots & \ddots & \vdots \\ u_m v_1 & u_m v_2 & \cdots & u_m v_n \end{bmatrix}$$

Thank you! Rlease ask your question! General and anness

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